

# Sensitivity Analysis of Aerosol Parameter Estimations with Measured Solar Direct and Diffuse Irradiance

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**Abstract**—Sensitivity analysis of aerosol parameter (refractive index which consists of real and imaginary parts, size distribution which is represented by Junge parameter) estimations with measured solar direct and diffuse irradiance is made. Through experiments with the measured solar direct and diffuse irradiance, it is found that the results from the sensitivity analysis is valid and adequate.

**Keywords**—Aerosol; Atmospheric optical depth; Solar irradiance; Solar direct; Solar diffuse; Aereole; Junge parameter; Size distribution; Real and imaginary parts of refractive index

## I. INTRODUCTION

The largest uncertainty in estimation of the effects of atmospheric aerosols on climate systems is from uncertainties in the determination of their microphysical properties, including the aerosol complex index of refraction that in turn determines their optical properties. The methods, which allow estimation of refractive indices, have been proposed so far [1]-[3].

Most of the methods use ground based direct, diffuse and aureole measurement data such as AERONET [4] and SKYNET [5]. The methodology for estimation of a complete set of vertically resolved aerosol size distribution and refractive index data, yielding the vertical distribution of aerosol optical properties required for the determination of aerosol-induced radiative flux changes is proposed [6].

The method based on the optical constants determined from the radiative transfer models of the atmosphere is also proposed [7]. Laboratory based refractive indices estimation methods with spectral extinction measurements are proposed [8],[9]. All these existing methods are based on radiance from the sun and the atmosphere.

Through atmospheric optical depth measurements with a variety of relatively transparent wavelength, it is possible to estimate size distribution, molecule scattering, gaseous transmission, ozone and water vapor absorptions, etc. so that refractive index might be estimated [10]-[14]. In order to assess the estimation accuracy of refractive index with the proposed method, sensitivity analysis is conducted with a variety of parameters of the atmosphere. In particular, observation angle dependency is critical for atmospheric optical depth measurements. Therefore, it is conducted to

assess influences due to observation angle on estimation accuracies of refractive index and size distribution. Similar researches are conducted and well reported [15]-[27].

The next section describes the proposed system followed by experiment. Then concluding remarks are described with some discussions.

## II. PROPOSED METHOD

### A. Radiative Transfer Function

Measured solar direct irradiance  $F$  on the ground is expressed in equation (1)

$$F = F_0 e^{-m_0 \tau_t} \quad (1)$$

where  $F_0$  denotes extraterrestrial solar flux,  $m_0$  denotes air-mass which can be represented as  $1/\cos(\theta)$  where  $\theta$  denotes solar zenith angle, and  $\tau_t$  denotes atmospheric optical depth which can be expressed in equation (2)

$$\tau_t = \tau_a + \tau_m = \tau_{as} + \tau_{aa} + \tau_{ms} + \tau_{ma} \quad (2)$$

where the first suffix  $t$ ,  $a$  and  $m$  denotes total atmosphere, aerosols and molecules, respectively while the second suffix  $a$  and  $s$  denotes absorption and scattering, respectively.  $F$  can be measured on the ground while  $F_0$  is well modeled by many researchers. On the other hand,  $m_0$  can be well determined which results in estimation of atmospheric optical depth. Atmospheric optical depth due to aerosol and molecule has to be estimated together with their absorption and scattering components.

Meanwhile, measured solar diffuse irradiance on the ground can be expressed in equation (3).

$$E(\theta_0, \varphi) = E(\vartheta) = F m_0 \Delta \Omega \{ \omega \tau_t P(\vartheta) + q(\vartheta) \} \quad (3)$$

where  $\varphi$  denotes the angle between solar azimuth and observation azimuth directions while  $\vartheta$  denotes azimuth and elevation angles. There is the following relation between both angles,

$$\cos(\vartheta) = \cos^2 \theta_0 + \sin^2 \theta_0 \cos \varphi \quad (4)$$

$\Delta \Omega$  denotes solid angle of the solar diffuse measuring instrument while  $\omega$  denotes single scattering albedo which can be represented as follows,

$$\omega = (\tau_{as} + \tau_{ms}) / \tau_{tk} \quad (5)$$

$P(\vartheta)$  and  $q(\vartheta)$  denotes scattering phase function and multiple scattering component, respectively.  $P(\vartheta)$  is expressed as follows,

$$P(\vartheta) = \{\tau_{ms}P_m(\vartheta) + \tau_{as}P_a(\vartheta)\}/(\tau_{ms} + \tau_{as}) \quad (6)$$

Because of the observation wavelength and molecule radius has the following relation,

$$\frac{\pi r_a}{\lambda} < 0.4 \quad (7)$$

molecule component of scattering can be expressed based on the Rayleigh scattering theory. Molecule component of scattering phase function  $P_m(\vartheta)$  can be expressed as follows,

$$P_m(\vartheta) = \left(\frac{3}{4}\right) (1 + \cos^2\vartheta) \quad (8)$$

Molecule scattering component of the atmospheric optical depth is represented as follows,

$$\tau_{ms} = \{0.008569\lambda^{-4}(1 + 0.0113\lambda^{-2} + 0.00013\lambda^{-4})\} \left(\frac{p}{p_0}\right) \left(\frac{T_0}{T}\right) \quad (9)$$

where  $\lambda$  denotes observation wavelength while  $p$  and  $p_0$  denotes atmospheric pressure on the ground, standard atmospheric pressure (1013.25 hPa), respectively. On the other hand,  $T_0$  and  $T$  denotes standard air-temperature on the ground (288.15 K) and air-temperature on the ground, respectively.

Meanwhile, observation wavelength and aerosol particle size has the following relation,

$$0.4 < \frac{\pi r_a}{\lambda} < 3 \quad (10)$$

Aerosol scattering is expressed based on the Mie scattering theory.

Aerosol scattering intensity is expressed as equation (11).

$$\beta_a(\vartheta) = \frac{r^2}{2\pi} \int_{r_{min}}^{r_{max}} \{i_1(\vartheta, x, \tilde{m}) + i_2(\vartheta, x, \tilde{m})\} n(r) dr \quad (11)$$

where  $i_1$ ,  $i_2$  denotes Mie scattering intensity function as the function of  $x$  of size parameter,  $\vartheta$ , and  $\tilde{m}$  of aerosol refractive index. On the other hand,  $n(r)$  denotes the number of aerosol particles of which the radius is  $r$  and is called as number of aerosol particle size distribution in unit of  $1/\text{cm}^2/\mu\text{m}$ .

$$n(r) = dN(r)/dr \quad (12)$$

The size parameter can be represented as follows,

$$x = \left(\frac{2\pi}{\lambda}\right) r \quad (13)$$

On the other hand, aerosol optical depth is represented as follows,

$$\tau_a = \int_{r_{min}}^{r_{max}} \pi r^2 Q_{ext}(x, \tilde{m}) n(r) dr \quad (14)$$

where  $Q$  is called as Extinction Efficiency Factor. Sometime, the following volume scattering size distribution is used.

$$v(r) = \frac{vd}{d \ln r} \quad (15)$$

There is the well-known relation between the number and volume of size distributions as follows,

$$v(r) = \frac{4}{3} \pi r^4 n(r) \quad (16)$$

Junge proposed the following size distribution function with Junge parameter  $\gamma$ ,

$$Cr^{-\gamma} = \frac{dn}{d \ln r} \quad (17)$$

In this paper, the Junge function of size distribution is used because of its simplicity with only one Junge parameter.

Let integral kernel functions be

$$K_{ext}(x, \tilde{m}) = \left(\frac{3}{4}\right) \frac{Q_{ext}(x, \tilde{m})}{x^3} \quad (18)$$

$$K(\vartheta, x, \tilde{m}) = \frac{3}{2} \frac{i_1(\vartheta, x, \tilde{m}) + i_2(\vartheta, x, \tilde{m})}{x^3}$$

Then

$$\beta_a(\vartheta) = \frac{2\pi}{\lambda} \int_{r_{min}}^{r_{max}} K(\vartheta, x, \tilde{m}) v(r) d \ln r \quad (19)$$

$$\tau_a = \frac{2\pi}{\lambda} \int_{r_{min}}^{r_{max}} K_{ext}(x, \tilde{m}) v(r) d \ln r \quad (20)$$

$$P_a(\vartheta) = \beta_a(\vartheta) / \omega_a \tau_a \quad (21)$$

Solar diffuse irradiance taking into account the multiple scattering in the atmosphere measured on the ground can be represented as follows,

$$L(\vartheta) = F_0 m_0 e^{-m\tau_t} \{(\tau_{ms} + \tau_{MS})P_m(\vartheta) + \tau_{as}P_a(\vartheta) + \tau_A P_m(0^\circ)\} \quad (22)$$

where  $(\tau_{ms}P_m(\vartheta))$  implies Rayleigh scattering component while  $(\tau_{MS})P_m(\vartheta)$  implies multiple scattering component in the atmosphere. On the other hand,  $\tau_{as}P_a(\vartheta)$  implies aerosol scattering component while  $\tau_A P_m(0^\circ)$  implies multiple scattering component in the atmosphere after the reflection on the ground. Solar diffuse flux can be expressed as  $L(\vartheta)$  multiplied by observation solid angle  $\Delta\Omega$ . Meanwhile,  $\tau_{MS}$  and  $\tau_A$  are expressed empirically as follows,

$$\tau_{MS} = 0.02\tau_{SS} + 1.2\tau_{SS}^2\mu_0^{-1} \quad (23)$$

$$\tau_A = \frac{A\tau_2}{1-A\tau_3} \quad (24)$$

where

$$\tau_{SS} = \tau_{ms} + \tau_{sa}$$

$$\mu_0 = \cos(\theta_0)$$

$$\tau_2 = 1.34\tau_{SS}\mu_0 \left\{1 + 0.22 \left(\frac{\tau_{SS}}{\mu_0}\right)^2\right\}$$

$$\tau_3 = 0.9\tau_S - 0.92\tau_{SS}^2 + 0.54\tau_{SS}^3$$

Therefore, the contribution of multiple scattering in the atmosphere is expressed as follows,

$$q(\vartheta) = \tau_{MS}P_m(\vartheta) + \tau_A P_m(0^\circ) \quad (25)$$

### B. Actual Radiative Transfer Equation Solving

The following much stable parameter is introduced,

$$R(\vartheta) = \frac{E(\vartheta)}{F_{m_0\Delta\Omega}} = \omega\tau_t P(\vartheta) + q(\vartheta) = \beta(\vartheta) + q(\vartheta) \quad (26)$$

Instead of  $E(\vartheta)$ ,  $R(\vartheta)$  does not have large influence due to calibration error of the measuring instrument for solar direct and diffuse irradiance.  $\omega\tau_t P(\vartheta)$  is replaced to  $\beta(\vartheta)$ . It is called single scattering intensity. Widely used aerosol parameter estimation method and software code is called Skyrad.Pack developed by Teruyuki Nakajima [11]. In the Skyrad.Pack ver.4.2, iteration method is used as follows,

$$\beta_a^{(1)}(\vartheta) = R_{mean}(\vartheta)$$

$$\beta_a^{(n+1)}(\vartheta) = R_{mean}(\vartheta) \beta_a^{(n)}(\vartheta) / R^{(n)}(\vartheta)$$

where (n) denotes the iteration number while  $R_{mean}(\vartheta)$  denotes the measured solar diffuse irradiance. This method is appropriate in the sense of optimization of single scattering albedo and flux, as well as contribution factor of the multiple scattering component. In order to estimated single scattering flux, we have to know aerosol refractive index and size distribution. Therefore, inverse problem solving method is needed for this. The proposed method uses Moore-Penrose generalized inverse matrix method. Volume vector  $v$  (r dimension) of unknown size distribution  $v^{(n)}(r)$  is assumed to be the matrix  $g$  which consists of a measured aerosol scattering flux  $\beta_a^{(n)}(\vartheta)$  and aerosol optical depth  $\tau_a^{(n-1)}$ . Then,

$$g = Gv + \varepsilon \tag{27}$$

where  $G$  denotes a linear multiple term matrix. Thus, the size distribution can be determined as follows,

$$v = (G^T G + \eta H)^{-1} A^T g \tag{28}$$

where  $H$  denotes a smoothing matrix while  $\eta$  denotes Lagrange multiplier.

### III. EXPERIMENTS

#### A. The Instrument and Data Used

POM-01 of sky-radiometer which allows measurements of solar direct and diffuse as well as aureole irradiance measurements is used. Fig.1 shows outlook and calibration coefficient trend of the POM-1. POM-01 is set up on the top of the 7th building of the Science and Engineering Faculty of Saga University (1 Honjo, Saga, 840-8502 Japan). POM-01 measures solar direct irradiance with sun tracking capability and solar diffuse irradiance with 50 different diffuse angles in maximum with the following 7 center wavelength, 315, 400, 500, 675, 870, 940, 1020 nm. 315 nm is ozone absorption band while 940 nm is water absorption band, respectively.



(a) Outlook

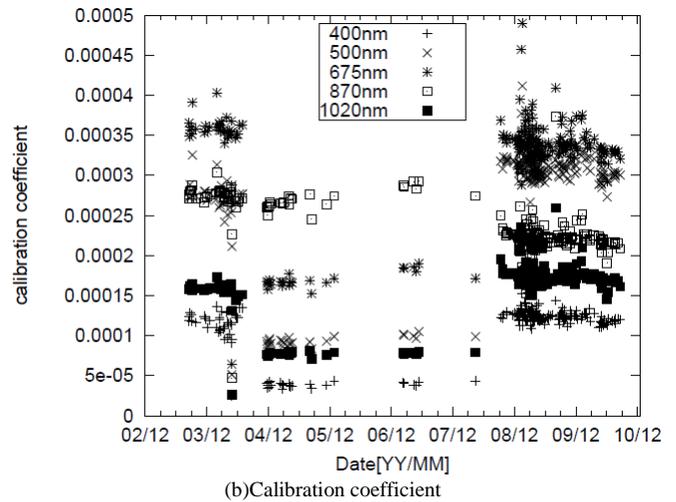


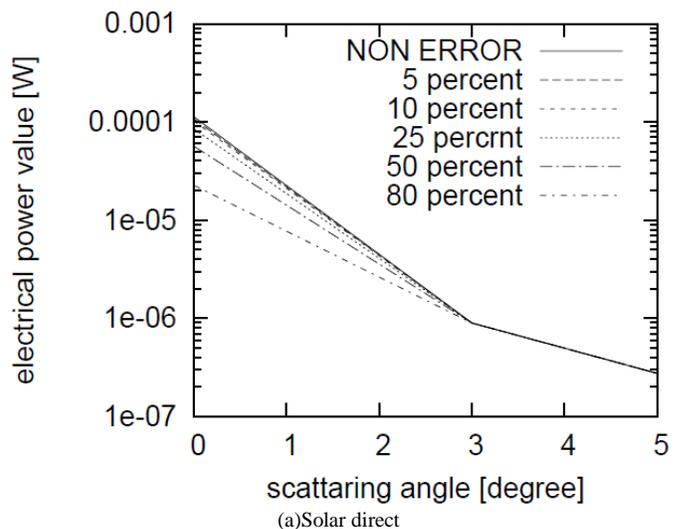
Fig. 1. Outlook and calibration coefficient trend of POM-01

POM-01 has self-calibration function. Using the function, calibration data is acquired routinely. Calibration coefficient trend can be divided into three periods, March 2003 to July 2004, July 2004 to October 2008, and October to now.

Fine weather condition of sky-radiometer data which is measured at 11:08 in the morning on May 25 2009 in the third period is selected due to the fact that calibration coefficients in the third period is relatively stable.

#### B. The Preliminary Experiments

The measured data for both solar direct and diffuse irradiances are in unit of output power. Firstly, the measured output powers are plotted as a function of scattering angle with the percent error of the solar direct in Fig.2. In accordance with increasing of solar direct angle error, the output power of POM-01 is getting down as shown in Fig.2 (a). Meanwhile, the output power of POM-01 decreases in accordance with increasing of solar diffuse angle error as shown in Fig.2 (b).



(a) Solar direct

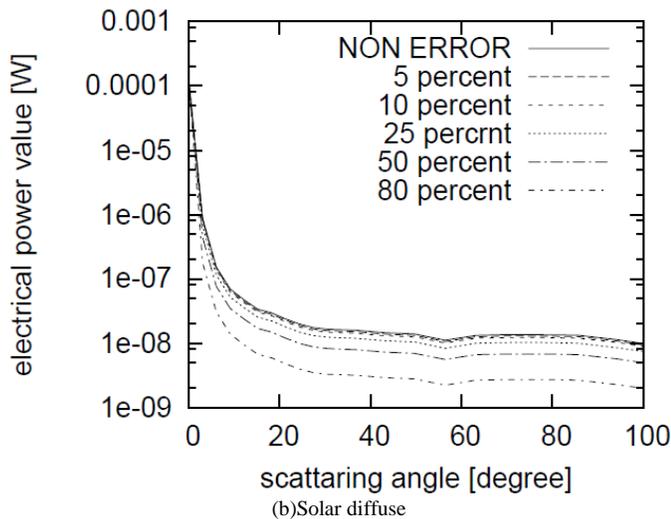


Fig. 2. POM-01 output power with pointing error on solar directions

On the other hand, skyrad.pack ver.4.2 allows estimation of volume spectral aerosol size distribution function. Using the relation between volume spectra and Junge size distribution function, equation (16), Junge parameter can be estimated based on the well-known least square method. Fig.3 shows the estimated Junge size distribution function for the aerosols on May 25 2009. It is found that the least square method does works for conversion from volume spectra to Junge distribution function with quit small error.

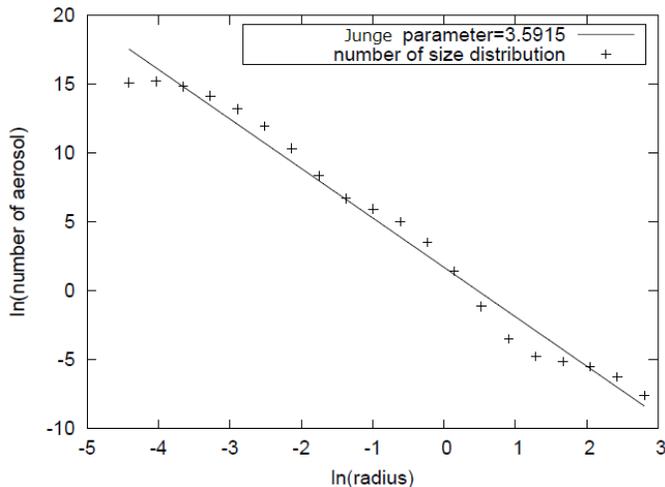


Fig. 3. Junge size distribution function of the aerosols on May 25 2009

The skyrad.Pack ver.4.2 requires the parameter for conversion, the number of iterations (NLOOP). In order to determine the parameter, the residual error is calculated as a function of NLOOP for the data which is acquired on May 25 2009. Fig. 4 shows the result. Fig.4 also shows the approximate function of residual errors which is expressed with the following function,

$$f(x) = ax^b \quad (29)$$

where  $a = 397.708$  and  $b = -1.602$ .

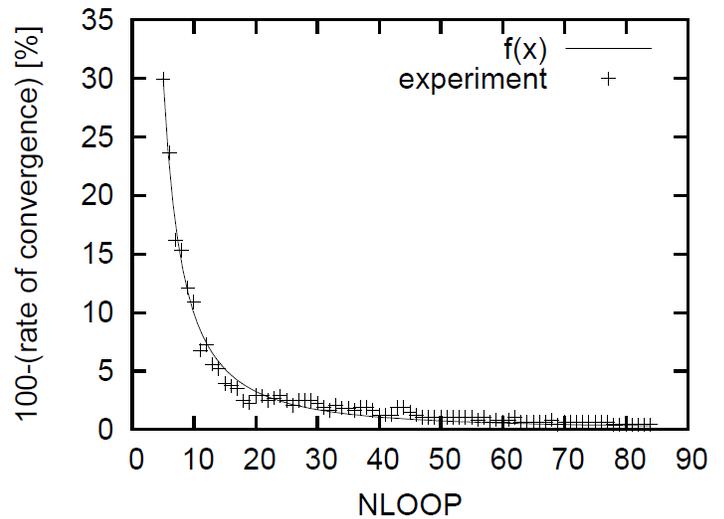
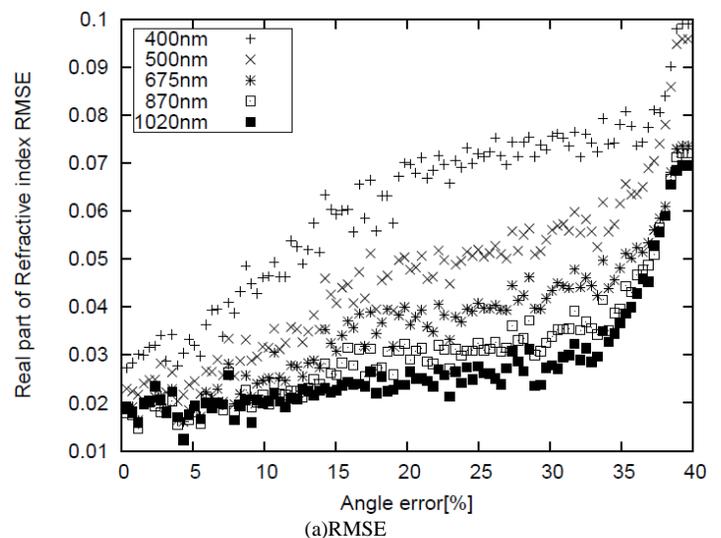


Fig. 4. Residual error (100-rate of convergence) as the function of the number of iterations (NLOOP)

### C. The Experimental Results

Using the modified skyrad.pack ver.4.2 described above, aerosol parameters, Real and Imaginary parts of aerosol refractive index and size distribution (Junge parameter) are estimated with the measured solar direct and diffuse irradiance which are measured with POM-01 on May 25 2009. Some of the errors are added on the solar direct angle and solar diffuse angle, respectively. Thus sensitivities of the pointing angle error on the estimated aerosol parameters are clarified.

Fig.5 shows the solar direct pointing angle error on the estimated real part of refractive index. The estimation error is evaluated with Root Mean Square Error: RMSE and percent error. As shown in Fig.5 (a) and (b), it is easily found that both of RMSE and percent error increases in accordance with increasing of solar direct pointing angle error. Also, it is found that both of RMSE and percent error increases in accordance with decreasing of wavelength.



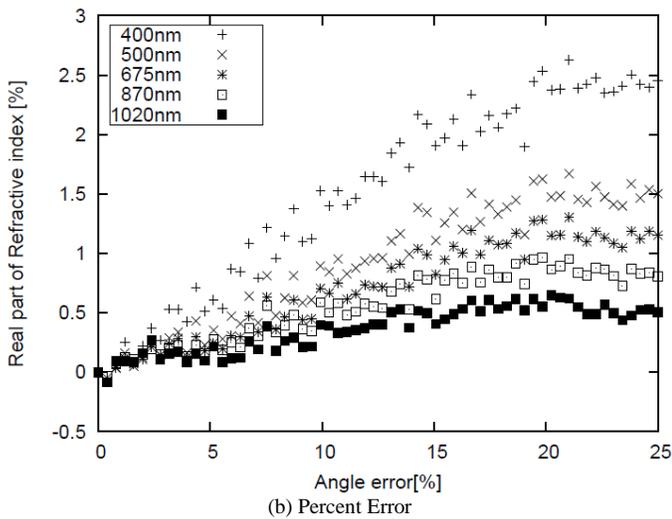


Fig. 5. RMSE and percent error of real part of refractive index caused by the solar direct angle error

On the other hand, Fig.6 shows the solar direct pointing angle error on the estimated imaginary part of refractive index. As shown in Fig.6 (a) and (b), it is easily found that both of RMSE and percent error increases in accordance with increasing of solar direct pointing angle error. Also, it is found that both of RMSE and percent error increases in accordance with decreasing of wavelength. RMSE and percent error of estimation error for real part of refractive index is much greater than that for imaginary part of refractive index obviously. Also, solar direct pointing angle error dependency on real part of refractive index is much smooth in comparison to that on imaginary part of refractive index. In other word, the estimated imaginary part of refractive index is much diverse than the estimated real part of refractive index. This is because of the actual real part of refractive index is much greater than that of imaginary part of refractive index.

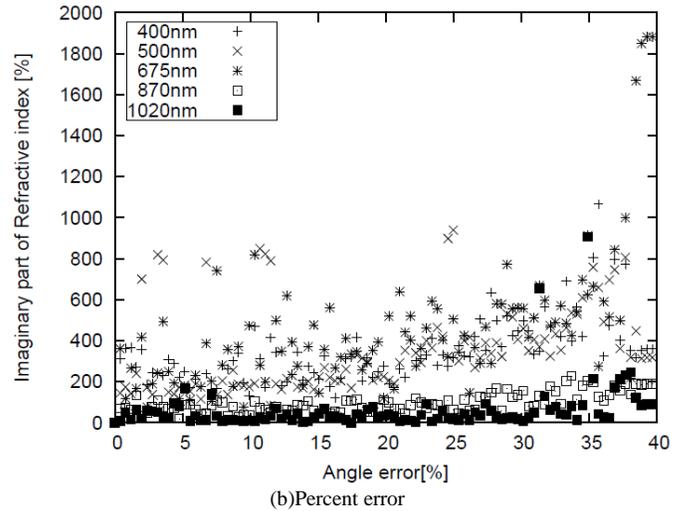


Fig. 6. RMSE and percent error of imaginary part of refractive index caused by solar diffuse angle error

Furthermore, it is found that RMSE of Junge parameter increases with increasing of solar direct pointing error as shown in Fig.7.

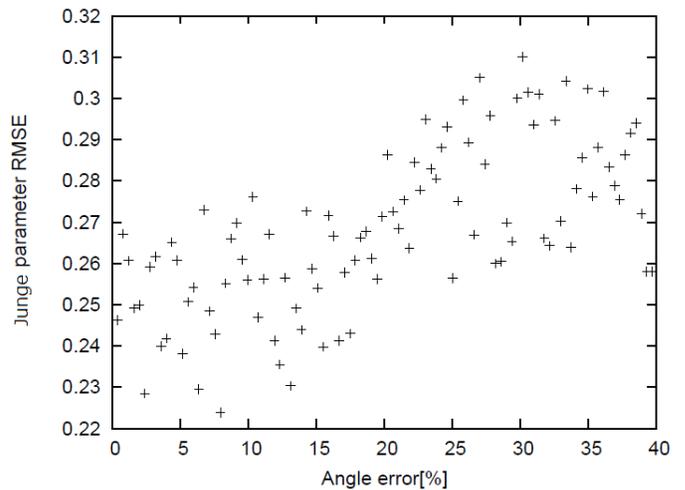
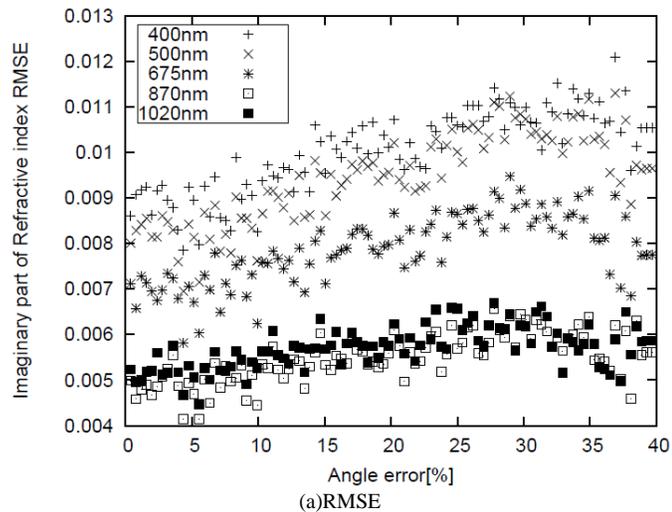


Fig. 7. RMSE of Junge parameter with the changing of solar direct pointing angle error



Meanwhile, Fig.8 (a) and (b) shows the solar diffuse pointing angle error on RMSE and percent error of the estimated real part of refractive index, respectively. As shown in Fig.8 (a) and (b), it is easily found that both of RMSE and percent error increases in accordance with increasing of solar diffuse pointing angle error. Also, it is found that both of RMSE and percent error increases in accordance with decreasing of wavelength.

On the other hand, Fig.9 shows the solar diffuse pointing angle error on the estimated imaginary part of refractive index.

As shown in Fig.9 (a) and (b), it is easily found that both of RMSE and percent error increases in accordance with increasing of solar diffuse pointing angle error. Also, it is found that both of RMSE and percent error increases in accordance with decreasing of wavelength. RMSE and percent error of estimation error for real part of refractive index is much greater than that for imaginary part of refractive index obviously. Also, solar diffuse pointing angle error dependency on real part of refractive index is much smooth in comparison to that on imaginary part of refractive index.

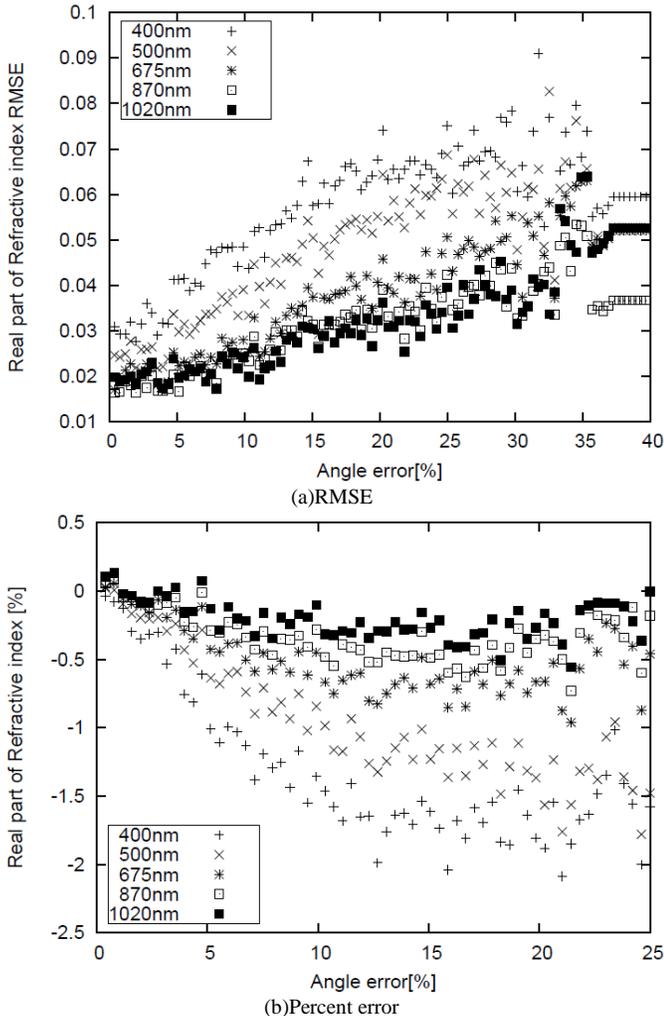


Fig. 8. RMSE and percent error of real part of refractive index caused by solar diffuse angle error

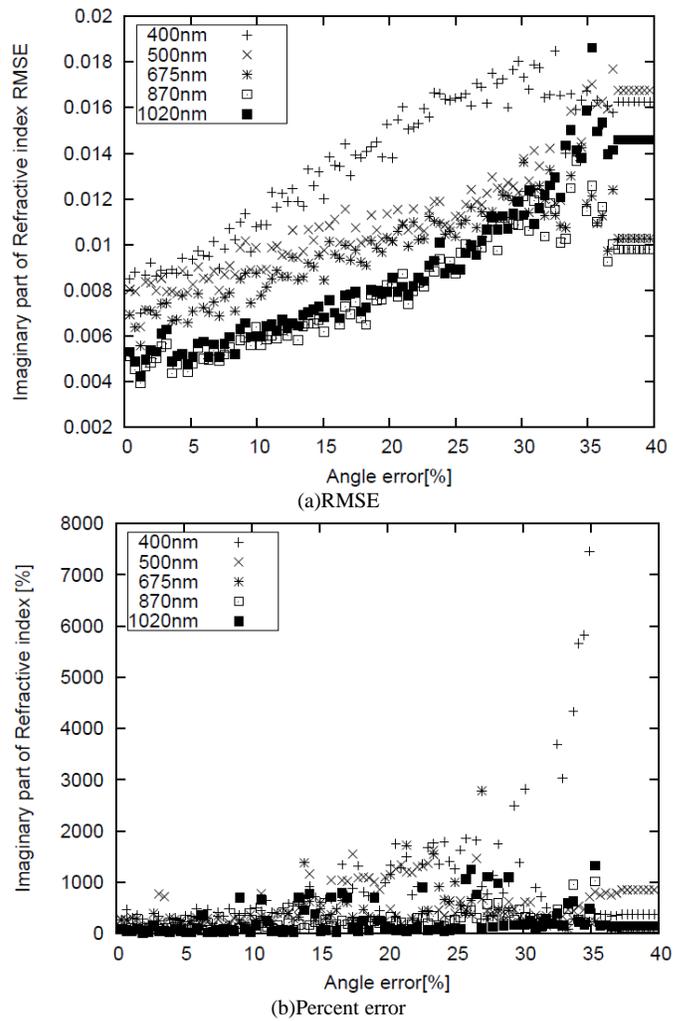


Fig. 9. RMSE and percent error of imaginary part of refractive index caused by solar diffuse angle error

In other word, the estimated imaginary part of refractive index is much diverse than the estimated real part of refractive index. This is because of the actual real part of refractive index is much greater than that of imaginary part of refractive index.

Furthermore, it is found that RMSE of Junge parameter increases with increasing of solar direct pointing error as shown in Fig.10.

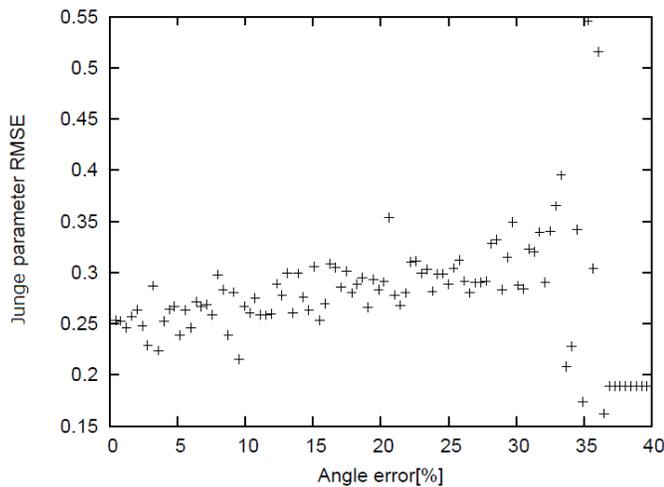


Fig. 10. RMSE of Junge parameter with the changing of solar diffuse pointing angle error

#### IV. CONCLUSION

Sensitivity analysis of aerosol parameter (refractive index which consists of real and imaginary parts, size distribution which is represented by Junge parameter) estimations with measured solar direct and diffuse irradiance is made. Through experiments with the measured solar direct and diffuse irradiance, it is found that the real part of refractive index estimation RMS error ranges from 0.01 to 0.035 which corresponds to 0.1 to 0.7 % error while RMSE of imaginary part of refractive index ranges from 0.004 to 0.0092 for less than 5 degree of the solar direct pointing angle error. On the other hand, it is also found that RMSE of the Junge parameter estimation error ranges from 0.22 to 0.269 for less than 5 degree of the solar direct pointing angle error.

Furthermore, it is found that the real part of refractive index estimation RMS error ranges from 0.017 to 0.036 which corresponds to 0.1 to 1.2 % error while RMSE of imaginary part of refractive index ranges from 0.004 to 0.0095 for less than 5 degree of the solar diffuse pointing angle error. On the other hand, it is also found that RMSE of the Junge parameter estimation error ranges from 0.23 to 0.29 for less than 5 degree of the solar diffuse pointing angle error. Therefore, pointing angle accuracy requirement for solar diffuse irradiance is little bit higher than that for solar direct irradiance.

Further investigations are required for the sensitivity analysis with the different characteristics of error (random number), not only for the uniformly distributed random number (this is used in this paper) but also the chi-square distribution of random number of error is taken into account.

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