

# Research on Islanding Detection of Grid-Connected System

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**Abstract**—This paper proposed a modified detection based on the point of common coupling (PCC) voltage in the three-phase inverter, combined over/under frequency protection, to achieve the detection of islanding states rapidly. Islanding detection is a common issue existing in distributed generation system. Compared with active islanding detection, this method could detect the islanding quickly and effectively. The simulation and experimental results shows that this new method can detect the islanding phenomenon quickly and accurately, which can meet the requirement of islanding detection standard, which ensure the stability of the system and the power quality recycling to the grid.

**Index Terms**—islanding detection; self-adaptive; active frequency shift; d-q transform

## I. INTRODUCTION

Islanding effect is also called Islanding phenomenon, the phenomenon is common in the photovoltaic grid-connected generation system. The power grid stop supplying the local load because of the fault or misoperation, however, the power system cannot detect it, still supplying the peripheral load, forming the power island out of the control of power grid.

Islanding effect will lead to serious results, such as disturbing the operation of the electricity system, destroying user devices, even severely endangered the life safety of the staff who is working for lines maintenance. Consequently, whether the condition of islanding can be detected effectively and timely or not is of great significant for the entire grid-connected system.

## II. MECHANISM AND DETECTION METHOD OF THE ISLANDING EFFECT

In a real world application, the load of the photovoltaic employs RLC parallel resonance circuit. According to the IEEE Std.929-2000 [1], the recommended generic system for islanding detection [2] study is shown in Fig.1.

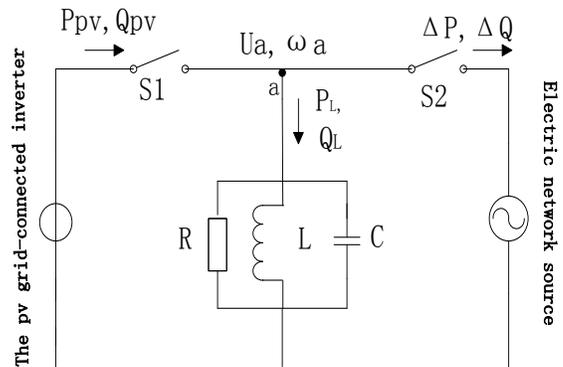


Fig. 1. System for islanding detection study

If the distributed grid-connected generation system works properly, namely

$$P_{pv} = P_L + \Delta P \quad (1)$$

$$Q_{pv} = Q_L + \Delta Q \quad (2)$$

$$P_L = \frac{U_a^2}{R} \quad (3)$$

$$Q_L = \left( \frac{1}{\omega_a L} - \omega_a C \right) U_a^2 \quad (4)$$

After the electric network cuts off the power, the photovoltaic grid-connected generation system generate islanding effect [3], namely

$$P_{pv} = P'_L = \frac{U_a'^2}{R} \quad (5)$$

$$Q_{pv} = Q_L' = \left( \frac{1}{\omega_a' L} - \omega_a' c \right) U_a'^2 \quad (6)$$

Eq (1), (3), (5) indicates that

$$U_a'^2 = U_a^2 + \Delta PR \quad (7)$$

Eq(2), (4), (6) indicates that

$$\left( \frac{1}{\omega_a' L} - \omega_a' c \right) U_a'^2 = \left( \frac{1}{\omega_a L} - \omega_a c \right) U_a^2 + \Delta PQ \quad (8)$$

Suppose  $U_a' = U_a'$ , plug (7) into (8), we can obtain:

$$(\omega_a - \omega_a')(1 + \omega_a \omega_a' LC) = \frac{\omega_a \omega_a' L \Delta Q}{U_a^2} \quad (9)$$

Where

$U_a$ 、 $\omega_a$ —Voltage and angular frequency of the load

$P_{pv}$ 、 $Q_{pv}$ —Output active power and reactive power of grid-connected systems

$\Delta P$ 、 $\Delta Q$ —Received active power and reactive power of the grid

$P_L$ 、 $Q_L$ —Received active power and reactive power of the grid

Eq(7), (9))indicates that, when the grid-connected generation system can not match with  $\Delta P$ , voltage of the load will change; when the grid-connected generation system can not match with  $\Delta Q$ , angular frequency will change. If the numerical value is big, voltage and angular frequency of the load exceeds the protected threshold of the over/under voltage and the over/under frequency, relay operates cut the connection between the grid-connected generation system and the grid, the grid-connected generation system will stop [4]. Conversely, if the numerical value is small, namely, voltage and frequency of the load changes in permissible range, islanding detection is failed, entering the non-detection zone(NDZ),the system operates in the island state The change threshold of the voltage and frequency of the load can be calculated from (10) and (11) respectively

$$\left( \frac{U}{U_{\max}} \right)^2 - 1 \leq \frac{\Delta P}{P_{PV}} \leq \left( \frac{U}{U_{\min}} \right)^2 - 1 \quad (10)$$

$$Q_f \left[ 1 - \left( \frac{f}{f_{\min}} \right)^2 \right] \leq \frac{\Delta Q}{P_{PV}} \leq Q_f \left[ 1 - \left( \frac{f}{f_{\max}} \right)^2 \right] \quad (11)$$

Where

$U_{\max}$ 、 $U_{\min}$ —The threshold of over/under voltage protection

$f_{50hz}$ 、 $f_{\min}$ —The threshold of over/under voltage protection

$Q_f$ —The quality factor of the RLC load.

Generally, according to whether to add artificial disturbance, there are two ways, passive and active methods. Passive method can complete test by monitoring the output AC voltage by inverter、frequency phase、harmonic instability, before and after the failure of the grid. The primary advantage to this approach is that it has no interference to the grid and the quality of the output electricity. The drawback of this approach is that it has large area of NDZ, when the load can not match with output power of the inverter. Over\unders frequency protection(OFP\UFP),Over\unders voltage protection(OVP\UVP), phase jump detection, voltage harmonic detection、active power change rate method、frequency change ratio methods are the most widely used passive islanding detection methods, which determine the islanding condition by measuring the PCC voltage and the current from the DG.

Active methods detect the effect on the line voltage by inject current frequency or phase interference signal in the output stage of the grid-side converter [5].

In the operation state of islanding, disturbance signals will accumulate on the line voltage and outside acceptable tolerances, thus detecting the islanding. Though active methods suffer smaller NDZS, the presence of disturbances during normal operation will sacrifice power quality and reliability of the power system. The sandia frequency drift [6], slip-mode frequency shift are three classical active methods by creating a continuous trend to change the frequency during islanding.

Based on the active islanding detection method for further analysis and comparison, a new and improved detection method is proved, namely, based on the d-q transform adaptive frequency shift(AFD) islanding detection method of the detection principle [7]-[10], by d-q transform on the point of common coupling(PCC) Voltage in the three-phase inverter, the output current of the inverter frequency periodic disturbance, combined over/under frequency protection, to achieve rapid detection of islanding states, which ensure the stability of the system and the power quality recycling to the grid.

### III. THE OPERATING PRINCIPLE OF AFP METHOD

#### A. AFD method

AFD is the most common method in the active islanding detection. The control flow of this method is presented in Fig 2.

Where

$f_{50hz}$ : the frequency of the grid voltage.

$f_{inv}$  :the output voltage frequency of the inverter

$\Delta f$  : the set value of frequency perturbation in the control system

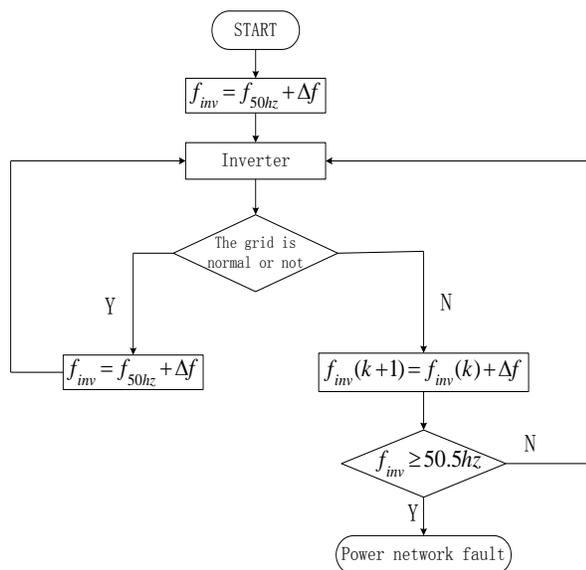


Fig. 2. Flowchart of the AFD method

Active frequency drift method works as follows:

Firstly, there are certain errors- $\Delta f$ , between the frequency of the output voltage and the grid voltage through the control of the inverter. Secondly,  $\Delta f$  is always within a narrow range because of the corrective action in the phase-locked loops circuit, when the grid operates properly [11]. Thirdly, the output voltage frequency of the inverter  $f_{inv}$  will change, when the grid failure. At the following power frequency periodic of the inverter, based on the  $f_{inv}$ , adding the set value of frequency perturbation to control the output voltage frequency of the inverter. It leads to the increasement of errors between output voltage frequency and the grid voltage frequency. The cycle continues after this, until output voltage frequency of triggering protection circuit [12], cutting the connection between inverter and the grid.

Fig 3 illustrate the waveform of the perturbation frequencies using AFD method. The curve describe the wave of current and interference signal in one power frequency periodic, plotted by time on the horizontal axis and per unit value of current on the vertical. The relations are as follows:

$$cf = t_z / T_{grid} \quad (12)$$

Where

$t_z$  : The period of the voltage value is zero.

$T_{grid}$  : A half cycle of the fundamental voltage

### B. The shortage of AFD method

As presented in [13],if the islanding occurs in the grid-connected generation system. There will be a much smaller

NDZS using AFD method than using passive detection methods. Once the value of  $cf$  is too small, compared with the traditional voltage frequency detection method, AFD method can not highlight its superiority; however, when the  $cf$  exceed the permitted value, the distortion ratio of current harmonic on AC grid side will increase, harmonics will affect the power quality recycling to the grid seriously. Therefore, NDZS in the AFD [14] would still need to be reduced in order to satisfy the increasing harsh conditions of the grid.

When the system load does not conform to (1), the system frequency will always beyond the normal range of work in theory. But, there is a time limit on detecting the islanding, especially the use of the automatic reclosing at present. If the detecting speed is too slow, the grid-connected generation system is not completely cut off before the automatic reclosing recloses again, it is very likely to make considerable oscillation, leading to accidents. Such a scenario may be typically in the AFD method, for example when the load is inductive, there is a trend that the phase of voltage is prior to current, the frequency of value will keep rising based on the assumption that without using AFD method, when the islanding happens [15]. However, if the value of  $cf$  is fixed in the AFD method, mitigating voltage frequency change, but tend to delay the trip time, and vice versa.

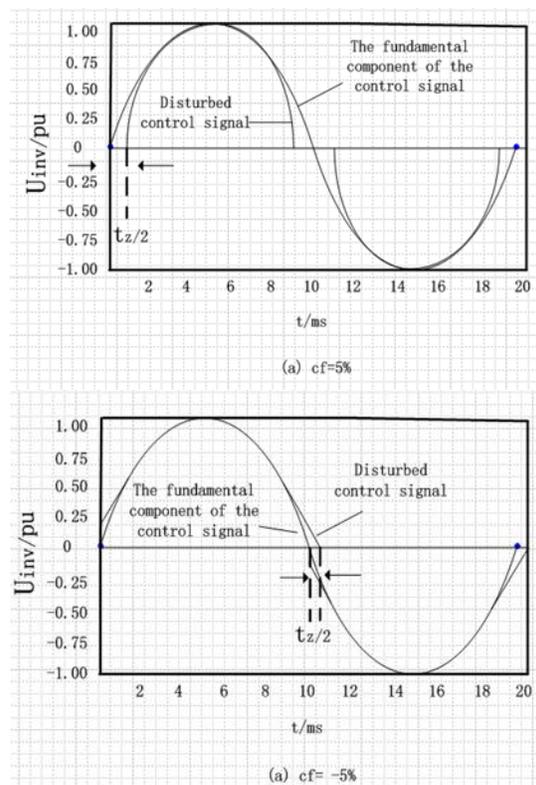


Fig. 3. Waveform of the perturbation frequencies using AFD method

### C. Adaptive Active Frequency Shift Islanding Detection Based on the d-q Transform

For overcoming the shortcomings of AFD method for islanding detection ,the detection algorithm of AFD method needs to be improved, convert the output current frequency disturbance of the inverter within single-phase into three-phase

grid-connected system. The new islanding detection algorithm-adaptive active frequency shift islanding detection based on the d-q transform will be available.

This method using the angle frequency after d-q transform in the positive feedback form at frequency disturbance. In this way, it will cause the three-phase output current frequency disturbance, achieving the adaptive active frequency shift islanding detection [16]-[18], Adaptive active frequency shift based on the d-q transform shown in the Fig 4.

Essentially, adaptive active frequency shift based on the d-q transform complete the control of islanding through the feedback structure. It refers to under the condition of different

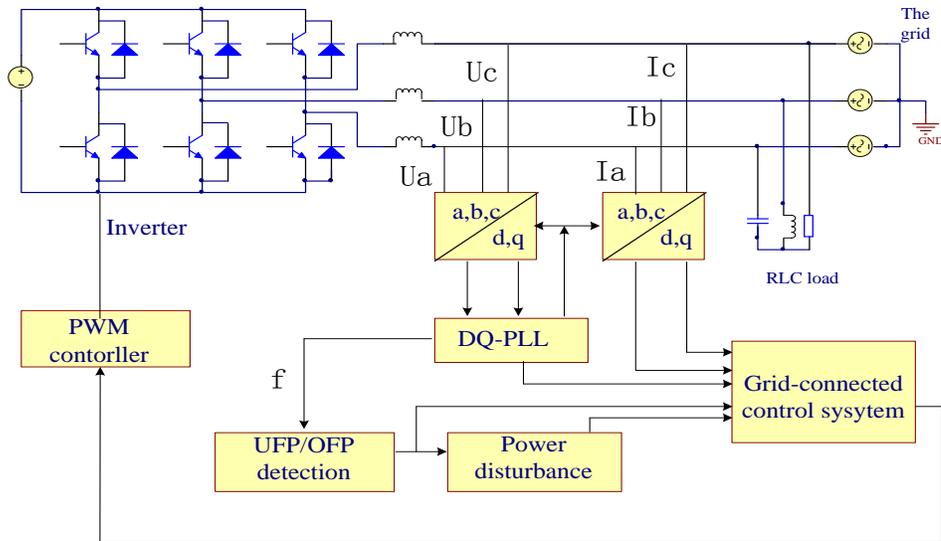


Fig. 4. Structure of improved design of is landing detection

Current frequency will take similar periodic disturbance, with the positive feedback control. The special algorithm processes are as follows:

$$f_i = \begin{cases} f_{up} + \Delta f, & f_{up} \geq 50\text{hz} \\ f_{up} + kn(f_{up} - 50), & f_{up} \leq 50\text{hz} \end{cases} \quad (15)$$

Where

$f_i$  : Output current frequency of inverter

$f_{up}$  : Frequency of PCC voltage

n: Positive feedback factor

k: Ratio coefficient

$\Delta f$  : Added frequency disturbance

During closing the switch of grid-connected, because of the clamp effect of the grid frequency, The PCC voltage follows the grid frequency. Although there are disturbances of current frequency during partial periodical, output current of the inverter, reset at the zero crossing point of the grid voltage, started with another sinusoidal. However, once the switch of the grid-connected is off, without the clamp effect of the grid

frequencies of inverter, using different methods to change the output current frequency [19]. The PCC voltage frequency is detected in every cycle, when the PCC voltage frequency exceed the normal frequency of the grid voltage-50hz, by applying a positive disturbance to the current frequency:

$$f_i = f_{up} + \Delta f \quad (13)$$

Conversely, if the PCC voltage frequency is less than 50hz, by applying a negative disturbance to the current frequency:

$$f_i = f_{up} - \Delta f \quad (14)$$

frequency, the PCC voltage will follow the change of the inverter output voltage [20].

Because of the effect of local load, the PCC voltage frequency will change accordingly, beyond the threshold value of frequency protection within the passive islanding detection, thus detect the islanding.

#### IV. SIMULATION RESULTS

In the end, the simulation model is put up using Matlab/Simulink. The output current of inverter is programmed in the S-Function module by using periodic frequency disturbance. Namely, add the adaptive active frequency shift based on the d-q transform, combined over/under frequency protection, to achieve rapid detection of islanding states. Three-phase grid voltage is 380V, grid frequency is 50hz, the threshold value of frequency protection is (50+0.5)hz.

According to the GB/T15945-1995, the allowable range of grid voltage frequency is 0.2hz, thus the value of it is 0.2hz. In the simulation, the value of  $\Delta f$  and k is 0.5 hz, and 5, respectively. The initial value of n is zero, increased by 2 every a periodical, increased frequency for quick detection. Continuous frequency perturbation for 3 cycles is added in the same algorithm every five periodicals. Select the balanced resonant load under the testing standard of islanding. In the load of the parallel RLC load, in order to achieve the

appropriate value of the quality factor-2.5, the value of L,C and R will be 61.5mh, 164.4 $\mu$ f, 48.39 $\Omega$ , respectively.

The simulation waveform are presented in Fig.3. It can be seen from the Fig5 that: the voltage wave of A-phase and grid-connected current without the adaptive active frequency shift based on the d-q transform. As the balanced load, the change of the current and voltage amplitude is very small, after disturbing electrical grids when the value of time is 50 ms. Using only OFP/UFM method can not detect the islanding. It can be seen from the Fig6 that: the output waveform of the current frequency.

Conversely, adding the adaptive active frequency shift based on the d-q transform to the islanding detection method, the frequency would drop off, until the value of frequency out of the threshold range of frequency protection, thus detect the islanding, meeting the testing time standard of islanding regulated by IEEEstd.1547.

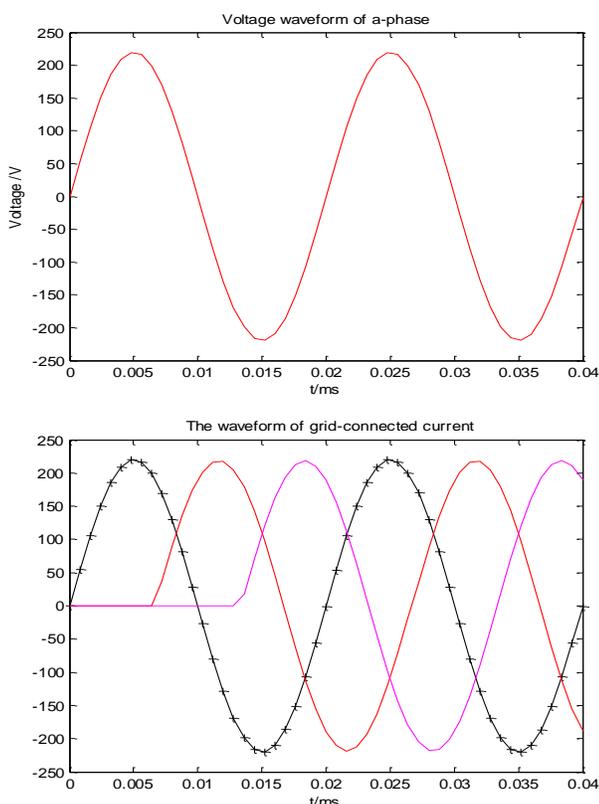


Fig. 5. Voltage waveform of a-phase and grid-connected current

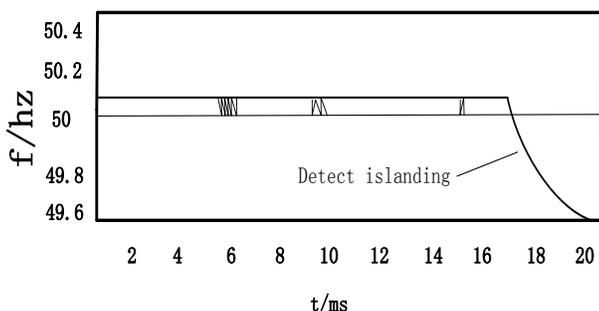


Fig. 6. Output waveform of the current frequency

## V. CONCLUSION

This paper proposed a modified detection based on the point of common coupling (PCC) voltage in the three-phase inverter, combined over/under frequency protection. The simulation results shows that this new method can detect the islanding phenomenon quickly and accurately, which can meet the requirement of islanding detection standard, which ensure the stability of the system and the power quality recycling to the grid.

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